

METHOD AND APPARATUS FOR IMPROVING THE MAGNITUDE OF COMPRESSIVE STRESS DEVELOPED IN THE SURFACE OF A PART

Background of the Invention

5 This invention relates to a method and an apparatus for performing the method of inducing compressive residual stress along the surface of a part and, more particularly, to a method and an apparatus for performing the method of burnishing or deep rolling a surface of a part whereby the magnitude and penetration of compressive residual stress achieved is
10 greater than that achieved by conventional burnishing.

 Surface residual stresses are known to have a major affect upon the fatigue and stress corrosion performance of components or parts in service. Tensile residual stresses that can be developed during manufacturing processes, such as grinding, turning, or welding are well known to reduce
15 both fatigue life and increase sensitivity to corrosion-fatigue and stress corrosion cracking in a wide variety of materials. It is also known that compressive residual stresses induced in the surface of a part can increase its fatigue life and reduce its susceptibility to corrosion-fatigue and stress corrosion cracking. However, the benefit of inducing a layer of surface
20 compression in reducing susceptibility to stress corrosion, cracking, fatigue, and corrosion-fatigue is lost if the layer of compression relaxes with time in service.

 Many components and parts of practical interest are subject to high tensile cyclic loads or high mean loads that often lead to fatigue, corrosion

fatigue, stress corrosion, or a combination of such failure modes. Therefore, it would be desirable to be able to introduce a layer of compressive residual stress along the surface of a part that will not relax significantly over time.

A method that has been developed and is widely used in industry to improve surface finish as well as fatigue life and corrosion resistance of a part by inducing a layer of compressive residual stress along its surface of the part is known as burnishing. During the burnishing process, the surface of a part is deformed by a rotary or sliding burnishing member that is pressed against the part in order to compress the microscopic peaks formed along the surface of the part into adjacent hollows. Burnishing thereby operates to develop compressive stresses by yielding the surface of the part in tension so that it returns to a state of compression following deformation. Burnishing tools comprising various wheel or roller burnishing member configurations have been developed for cold working a part and to induce a state of compressive stress and improved surface finish to the part. In addition, "deep rolling" and "low plasticity burnishing" processes have also been developed for producing deep layers of compressive stress that approach the yield strength of the material and which extend to over a millimeter into the surface. However, the deformation mechanism for producing such compressive stresses is based on hertzian loading and will generally produce maximum compression below the surface of the part. In many high strength or work hardening materials, the stresses produced along the upper surface by these burnishing methods can be far less than

the subsurface maximum, often being close to or having zero compression at the upper surface. Processes have therefore been developed to increase the stress levels at the upper surface of a part. Such processes include removing a thin layer of material from the surface of the part, such as by
5 etching, electropolishing, or some other non-tensile stress forming process; or a post treatment, such as shot peening, grit blasting, or similar compression producing treatments, to render the surface more highly compressive. Unfortunately, both approaches require a secondary surface treatment unrelated to the original burnishing process thereby adding time,
10 cost, and the potential for damage and the loss of the part during manufacture.

With respect to shot peening operations, secondary peening operations have been used to improve surface compression. For example, to increase the state of surface compression in a part, secondary peening
15 operations have been performed using small glass or ceramic shot following conventional steel shot peening with larger shot. Shot peening while being relatively inexpensive and preferred for many applications, is often unable to obtain the necessary coverage of the part without overlapping areas of impingement. Such overlapping often results in relatively large amount of
20 cold working which may leave the surface compressive layer susceptible to stress relaxation. Further, shot peening is often unacceptable for use in manufacturing parts requiring a superior finish, localized or relatively

complex compressive stress zones or patterns, or requiring a greater depth of compressive stress penetration.

Consequently, it would be desirable to have a relatively inexpensive and time efficient method and apparatus for implementing the method of improving the physical properties of a part by increasing the magnitude and penetration of compressive stress on the surface that would not significantly relax over time. It would also be desirable to have a method and an apparatus that would be effective for use with complex shaped surfaces and without detracting from the finish of the surface, and which could be performed relatively inexpensively and in a single pass.

Summary of the Invention

The novel method of the present invention for inducing compressive stress on the surface of a part comprises the steps of selecting at least one region along the surface of the part for inducing compressive surface stresses; performing a first operation to induce compressive surface stresses along the selected region of the part; and performing a second operation to induce a second layer of compressive surface stresses along the selected region of the part.

In another preferred embodiment of the invention the compressive surface stresses are induced into the selected region of the part by exerting compressive forces against the surface such that during the first operation the compressive force is greater than the compressive force exerted during the second operation.

In another preferred embodiment of the invention the first operation and the second operation of inducing compressive residual stresses along the surface of the part are burnishing operations.

5 In another preferred embodiment of the invention the burnishing operations are performed using a compression inducing means having a first burnishing member and a second burnishing member whereby the first burnishing member has a different modulus of elasticity than the second burnishing member.

10 In another preferred embodiment of the invention, the diameter of the first burnishing member is smaller than the diameter of the second burnishing member.

In another preferred embodiment of the invention the diameter of the first burnishing member is larger than the diameter of the second burnishing member.

15 In another preferred embodiment of the invention, the method induces at least one layer of compressive residual stress along the selected region such that the amount of cold working of less than about 5%.

In another preferred embodiment of the invention, the method induces at least one layer of compressive residual stress along the selected
20 region such that the amount of cold working of less than about 2%.

In another preferred embodiment of the invention, the second operation is performed as an independent secondary operation.

In another preferred embodiment of the invention, the first and the second operations are performed together in a single pass.

In another preferred embodiment of the invention, the first operation is performed while the selected region of the part is at a first temperature
5 and the second operation is performed while the selected region of the part being burnished is at a second temperature.

Another preferred embodiment of the invention, an apparatus for inducing compressive residual stress in the surface of a part comprises a first compression inducing means having a burnishing member and a
10 second compression inducing means having a burnishing member, wherein the burnishing member of the first compression inducing means has a diameter that is greater than or less than the diameter of the burnishing member of the second compression inducing means.

In another preferred embodiment of the invention, the apparatus for
15 inducing compressive residual stress in the surface of a part comprises a plurality of burnishing members having consecutively small diameters.

In another preferred embodiment of the invention, the first compression inducing means is fixed in a first positioning device and the second compression inducing means is fixed in a second positioning device.

20 In another preferred embodiment of the invention, the first compression inducing means and the second compression inducing means are fixed in a single positioning device.

In another preferred embodiment of the invention, the modulus of elasticity of the burnishing member of the first compression inducing means is different than the modulus of elasticity of the burnishing member of the second compression inducing means.

5 Various objects and advantages of the invention will be apparent from the following description, the accompanying drawings, and the appended claims.

Brief Description of the Drawings

To provide a more complete understanding of the present invention
10 and further features and advantages thereof, reference is now made to the following description taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a schematic representation of a preferred embodiment of the apparatus of the present invention for inducing a layer of compressive
15 residual stress in the surface of a part in which the means for inducing compression are fixed in a single positioning device effective for linear motion;

FIG. 2 is a schematic representation of the preferred embodiment of the apparatus of **FIG. 1** in which the means for inducing compression are
20 fixed in separate positioning devices;

FIG. 3 is a schematic representation of another preferred embodiment of the apparatus of the present invention for inducing a layer of compressive residual stress in the surface of a part in which the means for

inducing compression are fixed in a single positioning device effective for both linear and rotational movement;

FIG. 4 is a schematic representation of the preferred embodiment of the apparatus of **FIG. 3** in which the means for inducing compression are
5 fixed in separate positioning devices;

FIG. 5 is a schematic representation of the apparatus of **FIGS. 1** through **4** showing the relationships of the various components;

FIG. 6 is a flowchart illustrating a preferred embodiment of the method of the present invention for inducing a layer of compressive residual
10 stress in the surface of a part;

FIG. 7 is a graphical illustration of the subsurface residual stress distributions produced by the method of the present invention whereby a first operation was a burnishing operation performed using a 2.5 in. (6.35 cm) diameter ball and a second operation was a burnishing operation performed
15 using a .25 in. (0.64 cm) diameter ball to achieve compression of about 0.3 in (0.8 cm) into the surface of the part;

FIG. 8 is a graphical illustration of the subsurface residual stress distributions produced by the method of the present invention whereby the modulus of elasticity of the burnishing member used in the second operation
20 is higher than the modulus of elasticity of the burnishing member used in the first operation;

FIG. 9 is a graph illustrating that a greater depth of compression can be achieved with increase loading in spherical ball burnishing (using a 0.75

in (1.9 cm) ball) at an elevated temperature of 400 °F (204 °C) as compared to the same process at room temperature; and

FIG. 10 is a graph illustrating that an increase in surface tensile stress can be obtained by cooling the surface of the part (plotted as a function of the temperature differential between the surface and the interior of the part).

Detailed Description of the Invention

The present invention relates to a method and apparatus for performing the method of inducing compressive residual stress along a selected region of a part. In describing the preferred embodiments of the invention illustrated in the drawings, specific terminology will be resorted to for the sake of clarity. However, the invention is not intended to be limited to the specific terms so selected, and it is to be understood that each specific term includes all technical equivalents that operate in a similar manner to accomplish a similar purpose.

It has been found that the effect of secondary burnishing or deep rolling either parallel or perpendicular to the original path of the burnishing apparatus using the same burnishing member diameter and compressive loads have shown to have no significant effect on the residual stress developed. In order to facilitate the introduction of greater compressive residual stresses in a part, deep rolling and other conventional burnishing techniques have been developed that utilize multiple passes of the burnishing member over the surface of the part, often with an increasing

load, to induce compressive residual stresses within the surface. For parts where it is desirable to minimize cold working of the surface, low plasticity burnishing have been developed that performs the burnishing operation in a single pass and exhibits the same compressive residual stresses as
5 observed in conventional multi-pass burnishing.

It has now been unexpectedly found that if a smaller ball or roller diameter is used over the surface of a previously burnished part, that a much higher state of compressive stress can be generated on the upper surface of the part, eliminating the problem of low surface compression.
10 This process can be performed in stages with a single apparatus or using a series of burnishing apparatus having different size burnishing members, such as balls or rollers, whereby the burnishing members pass over the surface consecutively during a single pass or in multiple passes over the part.

15 Referring to **FIGS. 1** through **4**, there is illustrated an apparatus **100** for inducing a residual compressive stress in the surface **S** of a part **102**. According to one embodiment of the present invention, the apparatus **100** for inducing compressive residual stress along the surface **S** of a selected region of a part includes a first compression inducing means **104** and a
20 second compression inducing means **106**. While various compression tools have been developed for inducing a layer of residual compressive stress in the surface of a part, preferably, the first compression inducing means **104** and the second compression inducing means **106** preferably comprise

conventional burnishing members **108** and **110**, respectively. Various types of burnishing tools have also been developed, preferably the compression inducing means **104**, **106** are single-point burnishing members, such as described in U.S. Patent No. 5,826,453 entitled "Burnishing Method and Apparatus for Providing a Layer of Compressive Residual Stress in the Surface of a Workpiece," which is assigned to an assignee of the present invention and is incorporated herein by reference. As illustrated, in a preferred embodiment of the invention, the compression inducing means **104** and **106** each include a burnishing ball **112**, the forward most tip of which is caused to pass over the surface **S** of the part **102** in a rolling motion to induce deep compression. As schematically illustrated in **FIGS. 1** and **3**, the compression inducing means **104** and **106** are preferably mounted to a conventional single positioning device **114**, such as a robotic arm or milling machine (not shown). As schematically illustrated in **FIGS. 2** and **4**, the compression inducing means **104** and **106** are preferably mounted to conventional separate positioning devices **114**. Further, the burnishing members **108** and **110** may be mounted to a positioning device(s) **114** effective for linear motion, as shown in **FIGS. 1** and **2**, or to a positioning device(s) **114** effective for both linear and rotational motion, as shown in **FIGS. 3** and **4**.

The direction of motion and speed of the apparatus **100** and the first and second inducing means **104** and **106** will depend upon the material forming the part **102** and the final application of the part, as well as the

desired penetration of the residual compressive stress induced therein. The force applied by the compression inducing means **104** and **106** to the surface **S** of the part **102** will also depend on the desired penetration of residual compressive strength, material composition, material properties,
5 and dimensions of the part **102**, and the application of the final part.

The apparatus **100** of the present invention can be manually or automatically operated. Referring to **FIG. 1** and as schematically illustrated in **FIG. 5**, the apparatus **100** can include a controller **116** for automatically controlling the positioning device **114** and, thus, the direction of motion and
10 speed of the compression inducing means **104** and **106**. The controller **116** also can be used to control the force applied by the compression inducing means **104** and **106** to the surface **S** of the part **102**. The controller **116** can include a microprocessor, such as a computer operating under computer software control. In one embodiment, the positioning device **114** includes
15 belt and/or gear drive assemblies (not shown) powered by servomotors (not shown), as is known in the art. The controller **116** can be in operable communication with the servomotors of the positioning device **114** through suitable wiring (not shown).

One or more sensors **118**, including, but not limited to, linear variable
20 differential transformers or laser, capacitive, inductive, or ultrasonic displacement sensors, which are in electrical communication with the controller **116** through suitable wiring, can be used to measure the spacing of the compression inducing means **104** and **106** above the surface **S** of the

part **102**, and, thus, the motion of the compression inducing means **104** and **106**. Similarly, shaft encoders in servo systems, stepper motor drives, linear variable differential transformers, or resistive or optical positioning sensors can be used to determine the position of each compression inducing means

5 **104** and **106** along the surface **S** of the part **102**. One or more pressure sensors **120** including, but not limited to, load cells incorporating resistive, piezoelectric, or capacitive elements, which are in electrical communication with the controller **116** through suitable wiring, can be used to measure the amount of force applied by each of the compression inducing means **104**

10 and **106** to the surface **S** of the part **102**. For example, pressure transducers can be used to monitor the hydraulic pressure applied by a piston to determine the normal force on the compression inducing means **104** and **106**. The measurements obtained by the motion and pressure sensors are communicated to the controller **116**. The controller **116**

15 compares the measurements to preprogrammed parameters and, if necessary, instructs the servomotors (not shown) of the positioning device **114** to make corrections or adjustments to the direction of motion, speed of motion, and/or force being applied by the compression inducing means **104** and **106**.

20 When inducing compressive residual stress along a selected region on the surface **S** of a part, the part **102** is preferably secured to a work table (not shown) by means of a clamp or similar device (not shown). The apparatus **100** is positioned relative to the part **102** such that the

compression inducing means **104** and **106** are positioned adjacent to the surface **S** of the part **102**. The first compression inducing means **104** is engaged and moved along the surface of a part **102** to induce a first layer of compression within the surface **S**. According to another embodiment (not shown), the first compression inducing means **104** is fixed and the part **102** is moved relative to the compression inducing means **104**. Thereafter, the second compression inducing means **106** is engaged and moved along the surface **S** of the part **102** to induce residual compressive stress along the upper surface of the part **102**. According to another embodiment (not shown), the second compression inducing means **104** is fixed and the part **102** is moved relative to the second compression inducing means **104**. It should now be apparent that as shown in **FIGS. 1** and **3**, the first compression inducing means **104** and the second compression inducing means **106** can be fixed in a single positioning device **114** or can be fixed in separate positioning devices **114** as shown in **FIGS. 2** and **4**.

As discussed above, the first and the second compression inducing means **104** and **106** operate by forcing the burnishing member **110** against the surface **S** of the part **102** to produce the zones of deformation and to induce both residual compressive stresses deep within the surface as well as along the upper surface of part **102**. As previously described, in a preferred embodiment, the first compression inducing means **104** and the second compression inducing means **106** are attached to a shared positioning device **114** (**FIGS. 1** and **3**). As illustrated, the orientation and

positioning of the first and the second compression inducing means **104**, **106** are such that the second compression means **106** follows the same path of the first compression inducing means **104** thereby imparting additional compressive residual stresses within the surface **S** of the part **102**. In another preferred embodiment, the first compression inducing means **104** and the second compression inducing means **106** are attached to separate positioning devices **114** (**FIGS. 2 and 4**). In this way, the second compression inducing means **106** may follow the same path of the first compression inducing means **104** or may follow a different path and may therefore impart a more complex pattern of residual stresses within the surface **S** of the part **102**.

According to another embodiment of the present invention, conventional X-ray diffraction techniques are used to analyze the surface **S** of the part **102** to determine a selected region, the desired compressive stress pattern, penetration depth, as well as the amount of cold working and surface hardening necessary to optimize the material properties of the part **102**. The burnishing member **112** of each compression inducing means **104** and **106** can then be passed in a predetermined pattern with a constant or varying pressure, manually or using the controller **116**, across the surface **S** of the part **102** to induce the desired pattern of residual compressive stresses within the surface **S**.

Referring to **FIG. 6**, there is illustrated the method of inducing a layer of compression along the surface of a part, according to one embodiment of

the present invention. The method includes the steps of selecting at least one region of the surface of a part for inducing a deep layer of compressive residual stress therein, step **202**, and performing a first operation to induce a selected pattern of residual compressive stress within the region of the surface of the part, step **204**. The method further includes selecting the same region and/or another region(s) for inducing a more shallow layer of compressive stresses, step **206**, and performing a second operation to induce a second more shallow layer of compressive surface stresses along the selected region(s), step **208**. In a preferred embodiment of the invention, the method includes controlling the amount of cold working and surface hardening in the portion of the surface of the part. For example, in one embodiment, the desirable amount of cold working may be less than about five percent (5%) or less than about two percent (2%). In another embodiment, the method of inducing the layer of compressive residual stress is by burnishing. In another embodiment, the first and second operations are performed such that the means for inducing compression across the surface of a part are moved in a predetermined pattern and pressure to induce zones of residual compressive stress that do not substantially overlap. In another embodiment, the method includes performing X-ray diffraction to determine the optimum compressive stress pattern to be induced within the surface of the part, step **210**. In another embodiment, the first and the second operations are performed such that the direction of motion and/or the speed of motion of the means of inducing

compression across the surface of the part are controlled. In yet another embodiment, the method includes adjusting the force being applied by the means of inducing compression against the surface of the part, step 212.

The method of burnishing applied in a single-pass or in multiple
5 passes can be effective for producing compressive residual stresses following tensile deformation of the part along the upper surface of the part and to a certain depth within the surface of the part and produces deep compression with minimal cold working. It has been found that single-point burnishing can be used to produce a part with less cold work and surface
10 hardening than a part subjected to conventional burnishing operations. It has also been found that the layer of residual compressive stress developed, according to the present invention, penetrates to a greater depth than that developed by conventional burnishing. The amount of cold working and surface hardening also can be varied as part of the process to
15 optimize the material properties of the part. The optimal amount of cold working and surface hardening will depend on the particular material of the part and the environment which the part will be subjected to during its life. It has been found, however, that by cold working the surface of the part by less than about five percent (5%) and, more preferably, by less than about
20 two percent (2%), results in a part having longer retention of residual compressive stress at elevated temperature, less rapid relaxation under cyclic loading, and less alteration of the residual stress field during tensile or

compressive overload than parts formed using conventional cold working and surface hardening processes.

Referring to **FIG. 7**, a graphical representation illustrating the subsurface residual stress distributions produced by the method of the present invention is shown whereby the first operation for inducing compressive residual stress in the surface of the part was performed using a 2.5 in. (6.35 cm) diameter ball burnishing member and the second operation was performed using a 0.25 in. (0.64 cm) diameter ball burnishing member to achieve compression of about .31 in. (0.8 cm) into the surface of the part. The upper graph shows the residual stress distributions as functions of depth and shows the increased compression achieved to a depth of less than about one millimeter due to the use of the second pass burnishing operation.

Referring to **FIG. 8**, a graphical representation illustrating the subsurface residual stress distributions produced by conventional burnishing and by the method of the present invention is shown whereby conventional burnishing was performed for inducing compressive residual stress in the surface of the part using a .25 in. (.635 cm) diameter ball burnishing member in a single pass and the method of the present application by performing a first operation using a .25 in. (.635 cm) diameter burnishing member and a second operation using a 0.25 in. (0.64 cm) diameter ball burnishing member whereby the modulus of elasticity of the burnishing member used in the second operation is greater than the modulus of

elasticity of the burnishing member used in the first operation. As can be seen, the residual stress distributions as a function of depth shows the increased compression achieved to a depth of less than about one millimeter due to the use of the second pass burnishing operation.

5 It has also been found that by inducing a layer of compressive residual stress in the surface of a part, such as by burnishing, along regions having elevated temperature produces residual stresses that are more stable when subjected to elevated temperature. Such stability is believed to be attributed to strain aging which occurs during the warm deformation
10 process that leads to more diffuse dislocation structures and pinning of dislocations by solute atoms and/or precipitates. It has also been found that by performing the compression operation with the surface of the part heated to an elevated temperature, rather than at room temperature, produces a deeper compressive residual stress layer. Because of the reduction of the
15 part yield strength, plastic deformation extends to a greater depth thereby producing deeper compression, as well as deeper penetration of the burnishing tool, thereby producing more lateral flow of surface material and higher surface compression. Accordingly, the method of inducing a compressive residual stress along the surface of a part may include the step
20 of heating and/or cooling the surface prior to performing the first operation and/or prior to performing the second operation, step **214**. As illustrated in **FIG. 8**, the depth of compression, calculated using conventional finite element methods and published yield strengths, achieved by burnishing a

material, such as 7075-T6 aluminum, at a heated temperature, such as 400°F (204°C), is over twice the depth of compression achieved by burnishing at room temperature. The depth of compression achieved increases with the increasing burnishing load. It should now be apparent to
5 those skilled in the art that by performing a first operation at a first temperature and then a second operation at a second temperature can induce multiple layers of residual compressive stress or that various patterns of compressive residual stress can be induced along the surface of a part. Further, by performing the method of the present application using various
10 combinations of burnishing members having different diameters and/or different modulus of elasticity, burnishing patterns, and surface temperatures, numerous compressive residual stress patterns and layers can be induced within the surface of a part. It should also now be apparent to those skilled in the art that parts can now be manufactured or treated
15 having optimum compressive residual stress patterns that will improve fatigue life and reduce susceptibility to corrosion-fatigue and stress corrosion cracking. Further, by performing X-ray diffraction the optimum compressive stress pattern obtainable can be determined.

Accordingly, the method and the apparatus of the present invention is
20 a relatively inexpensive and effective means of inducing a desired layer of compressive residual stress in the surface of a part for providing the optimum fatigue life for reducing susceptibility to corrosion-fatigue and stress corrosion cracking.